

**In the Specification:**

1. On page 13, please amend the paragraph starting on line 14 with the following amended paragraph:

Fig. 3 shows a simplified basic diagram of a circuit arrangement 30 according to the prior art. A calibration resistance 11 is connected to an opener coil (not shown) of an injection valve of a high-pressure injection system for a diesel engine. It is connected on one side, by switching means ~~not shown~~18, to ground 15. On the other side it is connected to a series circuit of voltage divider resistors 321, 322 and 323 which is connected on one side to ground and on the other side via switching means ~~not shown~~18, to the +48 V supply voltage 33 of the on-board network. The circuit configuration shown is established by suitable control of the switching means to initialize the injection valves before the engine is started. Since the calibration resistance 11 is connected in parallel to the voltage divider resistances 321 and 322, a voltage divider circuit with resistor 323 on one side and resistors 321 and 322 on the other side is implemented with calibration resistor 11 as additional load resistance. The relationships produced here between the falling output voltage via resistors 321 and 322 as a function of the known input voltage and the calibration resistance to be determined are known to the person skilled in the art. In the circuit arrangement shown a further voltage divider is implemented since the output voltage used is tapped at the node between resistors 321 and 322. This measure is used to limit the output voltage to a range corresponding to the input range of the downstream analog multiplexer 34 (as a rule 0-5 V), and still enable the right resistance values for the calibration resistance in order of magnitude of appr. 1 a few 10 k $\Omega$  to be used. A further voltage limiting measure is realized by diode 16 which is connected against the 5 V-VCC supply voltage of the electronics. If the output voltage of the voltage divider circuit exceeds the permitted range of 0-5 V, the diode conducts so that the overvoltage will be limited and the inputs 341, 342 of multiplexer 34 are protected. The multiplexer switches the voltage at input 341 through to its output where the calibration voltage 14 is then present and is routed to a microcontroller (not shown) for further evaluation. After recording a calibration resistor the switching means switch to a next

calibration resistor and the corresponding voltage divider circuit of which the output voltage is then directed to a further input 342 of multiplexer 34. This procedure is repeated until all calibration resistors are recorded and microcontrollers can calculate the parameters required to control the individual valves or read them in from a memory. The engine can then be started. The disadvantages of this circuit arrangement have already been explained above.

2. On page 16, please amend the paragraph starting on line 25 with the following amended paragraph:

Fig. 5a shows an expansion of the circuit of Fig. 2 to control of a plurality of valves, in the present case of eight valves (not shown). A constant current source, in accordance with the particularly advantageous embodiment explained in Fig. 4 is used as a current source. As can be easily seen, the entire calibration network can be connected to the calibration resistor of interest in the most simple way with the switching resources ~~not shown~~18 able to be designed very simply and except for decoupling diodes 163a-h, all components of the calibration network only having to be simple designs. To improve clarity the calibration resistors to be connected to the decoupling diodes 163b-h are not shown in the diagram. The other components correspond to the relevant components with the same reference character in Figs. 1, 2 and 4.